



Date: 8/5/26

**2026 Glenwood Tank Site Projects:
Site Improvements (Secant Wall Installation)**

ADDENDUM NO. 2

The following clarifications and revisions are hereby incorporated in the Contract Documents, Construction Specifications and Plans for the project entitled, *"Glenwood Tank Site Project – Site Improvements (Secant Wall Installation), Scotts Valley Water District"*:

CONTRACT DOCUMENTS, CONSTRUCTION SPECIFICATIONS AND PLANS

CONTRACT DOCUMENTS:

Section 1 – Bid Documents: 1-C Bid Forms, Page 10,

Delete: Entire Page 10

Substitute: Revised Page 10 Attached

Perimeter Protective Fence has been changed to 6-feet tall (Item No. 3).

Secant Wall method of installation has been changed. A stem wall has been incorporated within the grade beam to accommodate the introduction of tie-backs. Stem Wall has been added to the Grade Beam bid section (Item No. 9).

The amount of un-reinforced concrete slurry pile depth has been increased. Depth of un-reinforced concrete slurry pile has been reduced with the introduction of tie-backs. Increase in amount has been reflected in Un-Reinforced Concrete Slurry Pile (Items No. 10).

The amount reinforced concrete pile has been increased. Depth of reinforced concrete pile has been reduced with the introduction of tie-backs. Size of rebar has been reduced within the footing from No. 14 vertical to No. 8 vertical. Increase in amount has been reflected in Reinforced Concrete Pile (Items No. 11).

Due to site constraints and an updated Geotechnical Report with updated seismic parameters the project was able to incorporate tie-backs to reduce the overall wall depth. Tie-backs, unit cost and quantity has been added as Post Tension Tie-Back Anchors (Items No. 12).

The new wall revision requires a bench to cut into the hill side for the tie-back caps to be exposed. This will require gabion basket to be installed at edges of slope to accommodate grade changes. Gabion basket and Grading, unit cost and quantity has been added as Gabion basket (Items No. 13).

CONTRACT PLANS:

Sheet C1.1 - Existing Site Plan & Demolition,

Revision: Delta 1 – Addendum No. 2 – Secant Wall Revision

Add: Barricade fence location and height

Original 4-foot fence is not high enough for site protection for the District. Protective fencing can be incorporated with new bench and gabion basket.

Sheet C2.1 - Site Improvement Plan,

Revision: Delta 1 – Addendum No. 2 – Secant Wall Revision

Add: Gabion baskets and excavating a bench on the exterior of the new Secant Wall.

Sheet C3.1 - Grading & Drainage Plan,

Revision: Delta 1 – Addendum No. 2 – Secant Wall Revision

Add: Grading of bench for new Secant Wall and revision to how the new storm pipe will connect to the existing outlet for the tank site.

Sheet S0.0 - Structural Specification Sheet,

Delete: Entire Sheet

Substitute: Revised Sheet S0.0 – Addendum 2 – Wall Revisions, dated 08-03-2026

Sheet S1.0 - Foundation Plan,

Delete: Entire Sheet

Substitute: Revised Sheet S1.0 – Addendum 2 – Wall Revisions, dated 08-03-2026

Sheet S2.0 - Foundation Plan,

Delete: Entire Sheet

Substitute: Revised Sheet S2.0 – Addendum 2 – Wall Revisions, dated 08-03-2026

Sheet S3.0 - Foundation Details,

Add: Entire Sheet

SPECIFICATIONS:

03 00 10 – Grade Beam,

Delete: Entire Specification

Substitute: 03 00 10 – Grade Beam and Stemwall Specification

03 00 40 - Post Tensioned Soil Tieback Anchors,

Add: Entire Specification

Added for payment description

31 51 13 - Post Tensioned Soil Tieback Anchors,

Add: Entire Specification

Wire Mesh Gabions and Mattresses Twisted or Welded Mesh,

Add: Entire Specification

GEOTECHNICAL REPORT:

Add: Technical Memo (Addendum No. 1) to original Geotechnical Report

Updated seismic parameters and slope stability analysis with new design criteria

Bid Schedule – Glenwood Tank – Site Improvements

Item No.	Description	Payment Reference	Unit	EST. QTY.	Unit Price	Extended Price
1	Mobilization	§3-A.01 G	LS	1		\$
2	Clearing and Grubbing	§3-A.03 F	LS	1		\$
3	Slope Safety (6-ft Barricade fence)	§3-A.04 E	LS	1		\$
4	Erosion Control	§3-A.06 E	LS	1		\$
5	AC Pavement (2-inches)	§3-D.12 E	SQ FT	1,270		\$
6	Storm Improvements	STORM - 1.2	LS	1		\$
7	Minor Concrete (Curb & Gutter)	§3-D.15 A	LF	113		\$
8	Chain-link Fencing	§3-D.21C (6)	LF	70		\$
9	Grade Beam & Stem Wall	03 00 10 – 1.02	LF	60		\$
10	Un-Reinforced Concrete Slurry Pile	03 00 20 - 1.02	EA	13		\$
11	Reinforced Concrete Pile	03 00 30 -1.02	EA	14		\$
12	Post Tension Tie-Back Anchors	03 00 40 -1.02	EA	14		\$
13	Gabion Basket & Excavation	Gabion -7.0	LS	1		\$
Total Bid Price					\$	

\$

(Written total of Contact Bid)

All bid entries must be filled in.

Addenda Received and Reviewed:

(Indicate with check marks in respective boxes)

Addenda Number and Date

Reviewed

The undersigned agrees that the enclosed cash deposit, cashier's check, certified check, or surety bond accompanying this bid shall be left on deposit with the District, that its amount is the measure of the liquidated damages which the District will sustain by the default of the undersigned through failure to execute and deliver the above agreement, insurance and bonds within ten (10) calendar days of written notice of the award of the contract and the money or surety bond so deposited by Contractor shall be collectible and become the property of the District in case of such default.

[illegible]

VICINITY MAP
SCALE: N.T.S.

SCOTT'S VALLEY WATER DISTRICT
2 CIVIC CENTER DRIVE
SCOTT'S VALLEY, CA 95066
OFFICE: 831.438.2363

C2G/CIVIL CONSULTANTS-GROUP, INC.
4444 SCOTTS VALLEY DRIVE, STE 600
SCOTTS VALLEY, CA 95066
OFFICE: 831.438.4420

R3 CONSULTING ENGINEERS
105 LOCUST STREET, STE A
SANTA CRUZ, CA 95060
OFFICE: 831.588.7628

GAS AND ELECTRIC:	PACIFIC GAS AND ELECTRIC
SANITARY SEWER:	CITY OF SCOTT'S VALLEY
STORM DRAIN SYSTEM:	CITY OF SCOTT'S VALLEY
WATER:	SCOTT'S VALLEY WATER DISTRICT

ALPHA SURVEY
4444 SCOTTS VALLEY DRIVE, STE 6
SCOTTS VALLEY, CA 95066
OFFICE: 831.438.4453

HARO, KASUNICH AND ASSOCIATES, INC.
116 EAST LAKE AVE
WATSONVILLE, CA 95076
OFFICE: 831.722.4175

105 LOCUST STREET, STE A
SANTA CRUZ, CA 95060
OFFICE: 831.588.7628

3. CONTRACTOR SHALL BE PERMITTED WITHOUT THE NEED FOR WRITTEN APPROVAL BY THE OWNER OR OWNERS REPRESENTATIVES AND THE SUBS TO REMOVE OR DESTROY ANY EVIDENCE OF VIOLATION OF THE PROHIBITED ACTS.

4. CONTRACTOR SHALL VERIFY LOCATIONS, ELEVATIONS AND DIMENTS OF EXISTING UTILITY PRIOR TO COMMENCEMENT OF WORK AND SHALL NOTIFY OWNERS OR OWNERS REPRESENTATIVES OF VIOLATIONS FOR THOSE SHOWN ON THE PLANS.

5. IF ANY REMAINS OF ARCHEOLOGICAL REMAINS ARE ENCOUNTERED DURING GRADING ACTIVITIES FOR ANY EQUIPMENT FOOTPRINT ON THE PROJECT, CONTRACTOR SHALL STOP WORK IMMEDIATELY AND NOTIFY THE OWNER AND THE CONSULTANT FOR AN ADJUSTED WORK PLAN. CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION AND RETENTION OF ANY REMAINS OF ARCHEOLOGICAL REMAINS IDENTIFIED TO DETERMINE THE NATURE OF THE DISCOVERY AND RECOMMEND APPROPRIATE EVALUATION PROCEDURES.

6. THE WORKER PLANS ARE CONSIDERED AS AN UNLAWFUL WORK IF CIVILICA CONSULTANTS GROUP, INC. HAS DEBARRED DESIGNER, CONTRACTOR, OWNER, AND/OR WHERE CREATED, OWNED AND DEVELOPED FOR OR IN CONNECTION WITH THE SPECIFIED PROJECT. NOTICE OF SUCH DEBARMENT SHALL BE OBTAINED FROM CIVILICA CONSULTANTS GROUP, INC. PRIOR TO THE COMMENCEMENT OF WORK. IF ANY OF THE ABOVE WHATSOEVER VIOLATES THE WRITTEN PERMISSION OF CIVILICA CONSULTANTS GROUP, INC. COPYRIGHT 2023 TOWNS OF CREMORA, D.B.A. CIVILICA CONSULTANTS GROUP, INC.

7. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL COORDINATION WITH THE APPROPRIATE UTILITY COMPANIES AND/OR AGENCIES TO VERIFY THE LOCATION AND DEPTHS OF ALL EXISTING UTILITIES PRIOR TO COMMENCEMENT OF WORK, AND SHALL NOTIFY CIVILICA OR A (303) 227-8665 AT LEAST 48 HOURS IN ADVANCE OF DISCUSSION.

CONTRACTOR AGREES THAT HE SHOULD ASSUME SOLE AND COMPLETE RESPONSIBILITY FOR JOB SITE CONDITIONS, INCLUDING THE SAFETY OF ALL PERSONS AND PROPERTY, DURING THE COURSE OF CONSTRUCTION OF THIS PROJECT, AND THAT REQUIREMENT SHALL APPLY CONTINUOUSLY AND NOT BE LIMITED DURING WORKING HOURS. THE CONTRACTOR SHALL DEFEND, INDEMNIFY AND HOLD THE OWNER AND THE DESIGN PROFESSIONALS HARMLESS FROM ANY AND ALL LIABILITY, REAL OR ALLEGED, IN CONNECTION WITH THE PERFORMANCE OF WORK ON THIS PROJECT, EXCEPTING FOR LIABILITY ARISING FROM THE SOLE NEGLIGENCE OF THE OWNER OR DESIGN PROFESSIONAL.

UNDERGROUND FACILITIES AND UTILITIES HAVE BEEN SHOWN BASED ON RECORD DRAWINGS AND VISIBLE EVIDENCE FOUND IN FIELD. NO WARRANTY IS MADE REGARDING THE COMPLETENESS OR ACCURACY OF SUCH INFORMATION. PRIOR TO CONSTRUCTION, DETERMINE THE EXACT LOCATION OF UNDERGROUND FACILITIES AND UTILITIES AND PRESERVE SAME FROM DAMAGE. PRIOR TO CONSTRUCTION, VERIFY LOCATION AND ELEVATION OF EXISTING UNDERGROUND UTILITIES AT THE CROSSING POINTS WITH PROPOSED UTILITIES. THE CONTRACTOR SHALL NOTIFY THE OWNER OR OWNERS REPRESENTATIVES IF CONDITIONS DIFFER FROM THOSE SHOWN ON THE DRAWINGS AND SHALL NOT BEGIN CONSTRUCTION UNTIL THE CHANGED CONDITIONS HAVE BEEN EVALUATED. CONTACT UNDERGROUND SERVICES ALERT (USA) (1-800-327-3600) TWO (2) WORKING DAYS PRIOR TO DIGGING. REPAIR UNDERGROUND UTILITIES DAMAGED BY CONSTRUCTION OPERATIONS. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL DAMAGES ASSOCIATED WITH CONTRACTOR'S FAILURE TO EXACTLY LOCATED AND PRESERVE UNDERGROUND FACILITIES AND UTILITIES.

IF THERE ARE ANY DISCREPANCIES BETWEEN THE CONSTRUCTION DOCUMENTS AND EXISTING CONDITIONS WHICH WILL AFFECT THE WORK, THE CONTRACTOR SHALL BRING SUCH DISCREPANCIES TO THE DESIGN PROFESSIONAL FOR ADJUSTMENT BEFORE PROCEEDING WITH THE WORK. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROPER FITTING OF ALL WORK AND FOR THE COORDINATION OF ALL TRADES, SUBCONTRACTORS, AND PERSONS ENGAGED UPON THIS CONTRACT.

CONTRACTOR SHALL BE RESPONSIBLE FOR ALL COORDINATION WITH THE APPROPRIATE UTILITY COMPANIES AND/OR AGENCIES TO VERIFY THE EXISTENCE AND/OR LOCATION OF ALL UNDERGROUND UTILITIES PRIOR TO COMMENCEMENT OF WORK, AND SHALL NOTIFY U.S.A. @ (800) 227-2600 AT LEAST 48-HOURS IN ADVANCE OF EXCAVATION.

CONTRACTOR IS RESPONSIBLE TO PROVIDE ALL SURVEYING AND OR STAKING BY A LICENSED SURVEYOR FOR ALL CONSTRUCTION PURPOSES.

AC	ASPHALT CONCRETE
BFP	BACK FLOW PREVENTER
BFW	BOTTOM FACE OF WALL
CB	CATCH BASIN
CL	CENTERLINE
CONC	CONCRETE
DI	DROP INLET/DEITCH INLET
DIP	DUCTILE IRON PIPE
ED	EDGE OF CEMENT
EP	EDGE OF PAVEMENT
EG	EXISTING GRADE
(E)	EXISTING
FF	FINISH FLOOR
FG	FINISH GRADE
FL	FLOW LINE
GS	GRADE GRADE
HP	HIGH POINT
INV	INVERT
LP	LOW POINT
MS	MATCH EXISTING
MSN	MANHOLE
PL	PROPERTY LINE
PSE	PUBLIC SERVICE EASEMENT
ROW	RIGHT OF WAY
TBW	TOP BACK OF WALL
TC	TOP OF CURB
TW	TOP OF WALL
TY	TYPICAL
WV	WATER VALVE

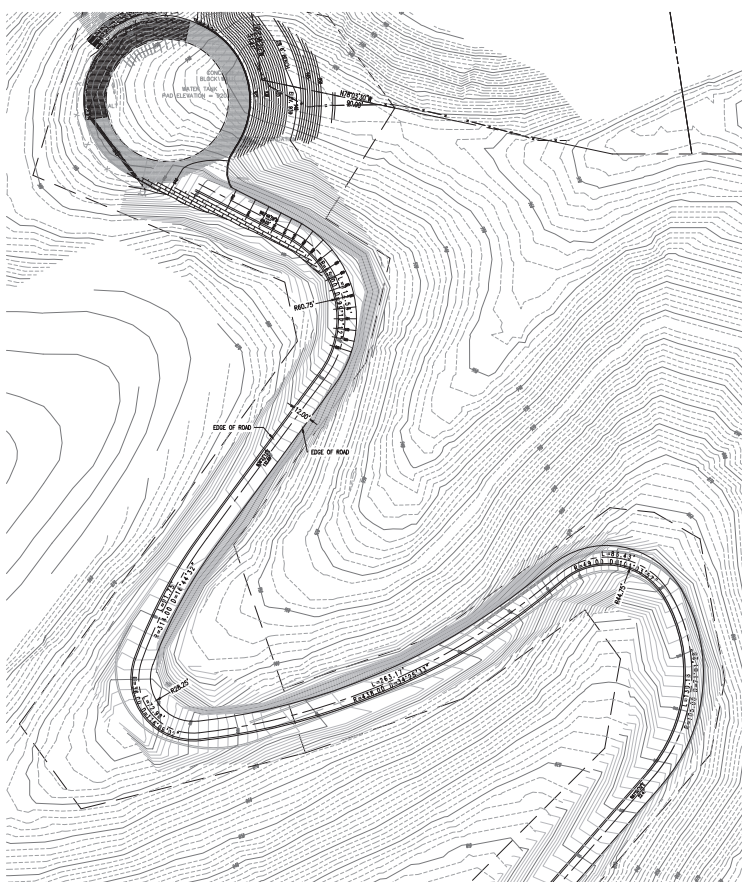
CD.1 - COVER SHEET
CD.2 - OVERVIEW SHEET
C.1 - EXISTING SITE/DEMOLITION PLAN
C.2 - SITE IMPROVEMENT PLAN
C.3 - GRADING AND DRAINAGE PLAN
C.4 - EROSION CONTROL PLAN

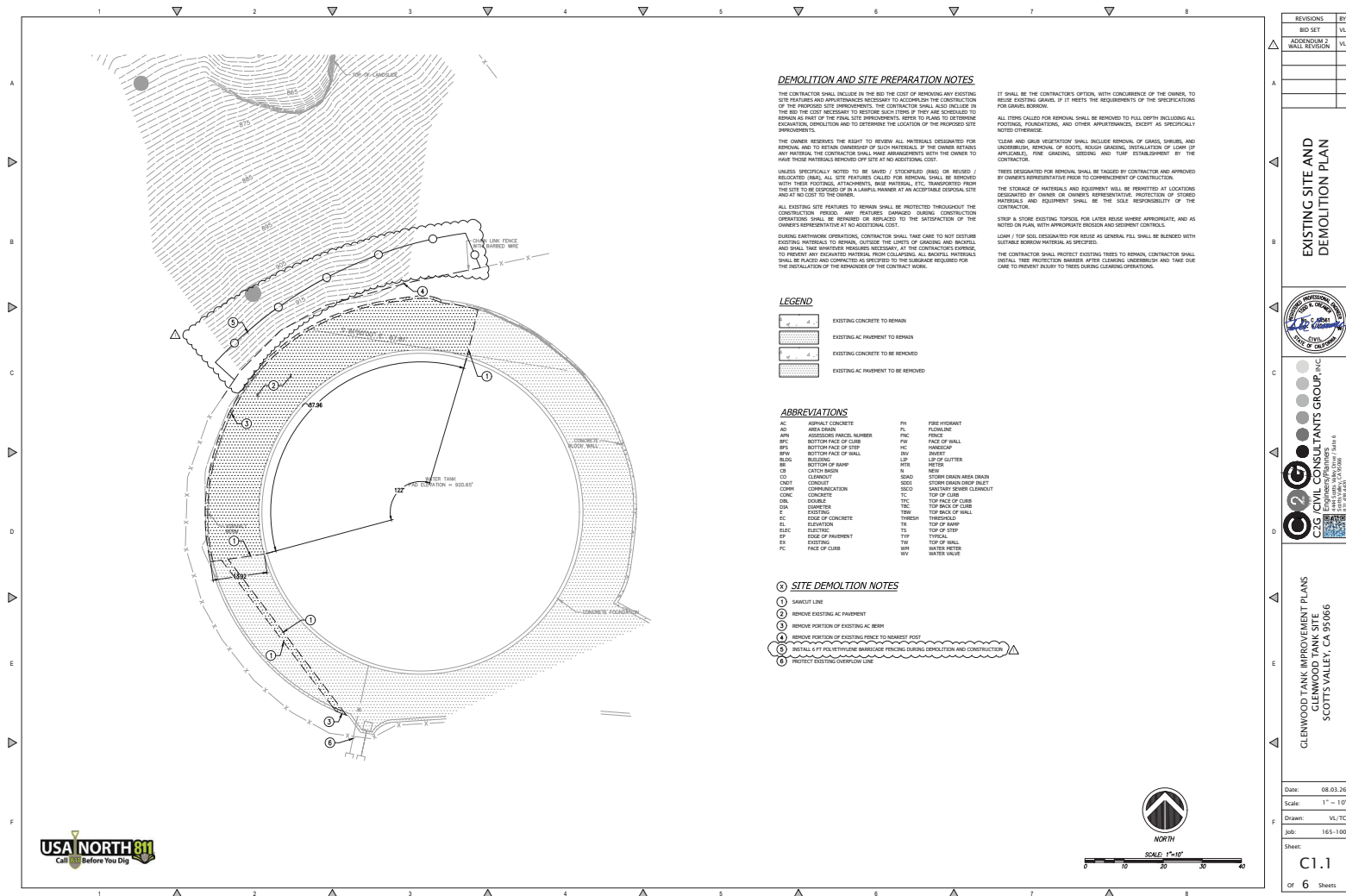
STRUCTURAL SHEET

S0.0 - STRUCTURAL SPECIFICATIONS
S1.0 - FOUNDATION PLAN
S2.0 - WALL SECTION
S3.0 - FOUNDATION DETAILS



SCALE: 1"=30'

[illegible]



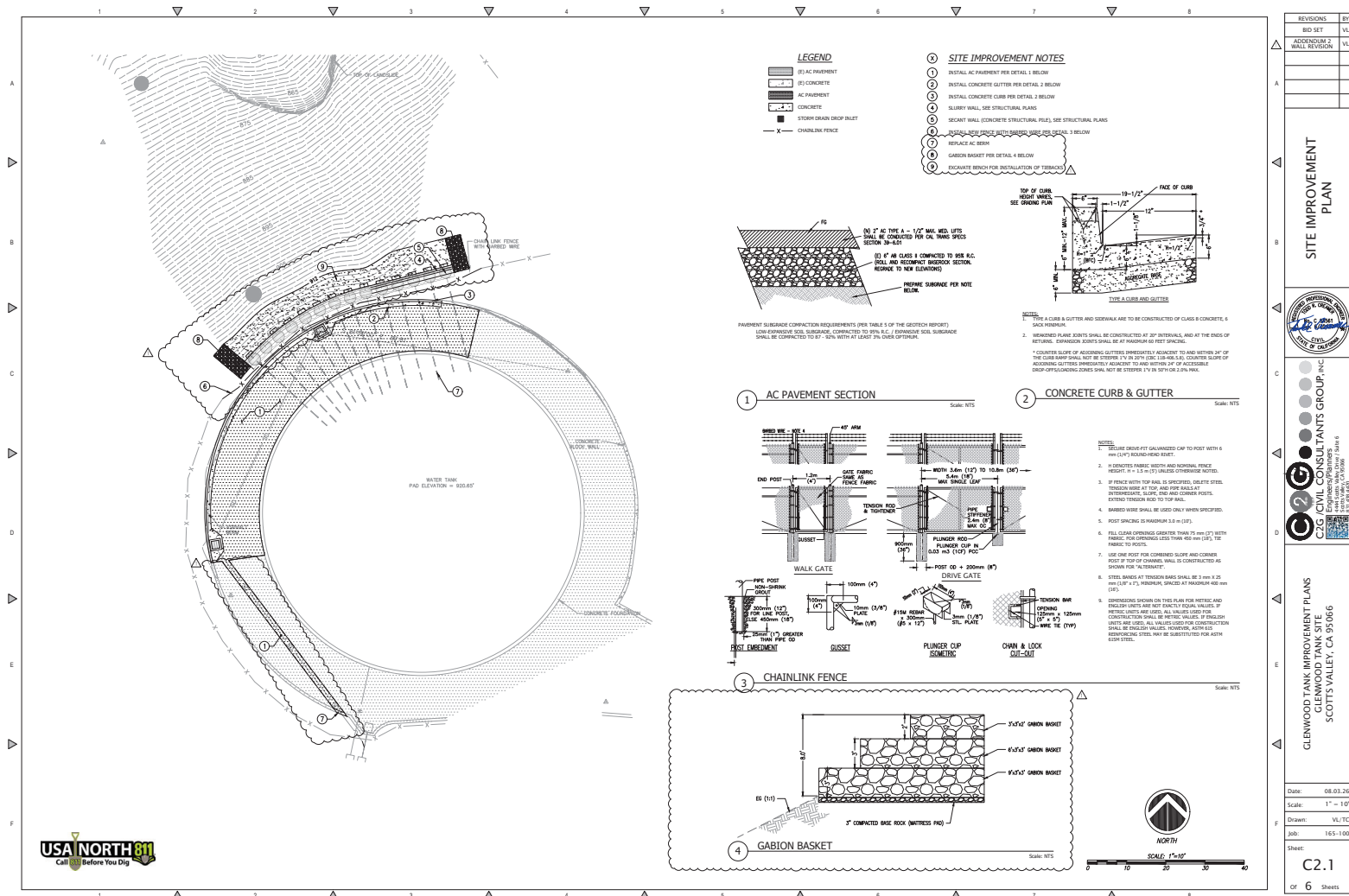
REVISIONS	BY
BID SET	VL
ADDENDUM 2 WALL REVISION	VL

EXISTING SITE AND DEMOLITION PLAN



GLENWOOD TANK IMPROVEMENT PLANS
GLENWOOD TANK SITE
SCOTT'S VALLEY, CA 95066

Date:	08.03.26
Scale:	1" = 10'
Drawn:	VL/TC
Job:	165-100
Sheet:	
	C1.1
	Of 6 Sheets







1 TIE BACK RETAINING WALL PLAN
SCALE: 1"=1'-0"



FOUNDATION NOTES:

1. REFER TO STRUCTURAL SPECIFICATIONS AND TYPICAL STRUCTURAL DETAILS SHEET S0.8.
2. DIMENSIONS ARE TO FACE OF CONCRETE, CENTERLINE FOOTING AND POSTS, ETC., UNLESS NOTED OTHERWISE. NOTIFY ARCHITECT OF ANY DISCREPANCIES. VERIFY ALL DIMENSIONS WITH ARCHITECTURAL PLANS BEFORE BEGINNING WORK.
3. THE GEOTECHNICAL ENGINEER SHALL BE RETAINED TO PROVIDE OBSERVATION AND TESTING SERVICES DURING THE GRADING AND FOUNDATION PHASE OF CONSTRUCTION FOR GEOTECHNICAL REPORT RECOMMENDATIONS AND INSPECTION AND TESTING REPORTS SHALL BE SUBMITTED TO THE BUILDING DEPARTMENT.



HILLTOPS OF CALIFORNIA PROJECT FOR THE
GLENWOOD TANK SITE
SCOTT'S VALLEY, CA 95066
FOUNDATION PLAN

REVISIONS	DATE	DESCRIPTION
1	06/04/2026	06/07/2026
2	06/04/2026	06/07/2026
3	06/04/2026	06/07/2026
4	06/04/2026	06/07/2026
5	06/04/2026	06/07/2026
6	06/04/2026	06/07/2026
7	06/04/2026	06/07/2026
8	06/04/2026	06/07/2026
9	06/04/2026	06/07/2026
10	06/04/2026	06/07/2026



1. THE ENGINEER HAS REVIEWED THE PROJECT AND FOUND IT TO BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE CALIFORNIA ENGINEERING ACT AND THE RULES AND REGULATIONS OF THE BOARD OF ENGINEERS AND SURVEYORS. THE ENGINEER HAS REVIEWED THE PROJECT AND FOUND IT TO BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE CALIFORNIA ENGINEERING ACT AND THE RULES AND REGULATIONS OF THE BOARD OF ENGINEERS AND SURVEYORS. THE ENGINEER HAS REVIEWED THE PROJECT AND FOUND IT TO BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE CALIFORNIA ENGINEERING ACT AND THE RULES AND REGULATIONS OF THE BOARD OF ENGINEERS AND SURVEYORS.

DATE: AUGUST 3, 2026
PROJECT: 1031-C-25-GL

S1.0

SECTION 03 00 10 – CONCRETE GRADE BEAM AND STEM WALL

PART 1 - GENERAL

1.01 RELATED DOCUMENTS:

- A. Structural drawings sheets S0.0, S1.0, S2.0 and S3.0
- B. General provisions of Contract Agreement form, including appendices and exhibits.
- C. Section 03 11 00 – Concrete Forming and Accessories
- D. Section 03 21 00 – Reinforcement Bars
- E. Section 03 30 00 – Cast-in-place Concrete
- F. Section 03 35 00 – Concrete Finishing

1.02 PAYMENT

- A. This section includes the following:
 - 1. Concrete Grade Beam and Stemwall: The Bidder shall include in its proposal all labor, materials, equipment, supervision, layout, forming, reinforcing steel coordination, concrete placement, finishing, curing, and incidental work required for the complete installation of the reinforced concrete grade beam. The Bidder shall include all costs associated with coordinating and integrating the vertical pier reinforcing steel into the grade beam, including proper alignment, lap splices, dowels, development lengths, concrete cover, reinforcing support, field adjustments, and coordination with the drilled pier/secant pile installation. No additional compensation shall be provided for work required to properly connect, embed, develop, or otherwise integrate the vertical pier reinforcing into the grade beam unless specifically approved in writing by the Owner prior to performance of the work.

SECTION 03 00 40 – POST TENSIONED SOIL TIEBACK ANCHORS

PART 1 - GENERAL

1.01 RELATED DOCUMENTS:

- A. Structural drawings sheets S0.0, S1.0, S2.0 and S3.0
- B. General provisions of Contract Agreement form, including appendices and exhibits.
- C. Section 31 51 13 – Post Tensioned Soil Tieback Anchors

1.02 PAYMENT

- A. This section includes the following:

- 1. Post-Tensioned Soil Tieback Anchors: The Bidder shall include in its proposal all costs associated with the complete installation of the post-tensioned soil tieback anchors, including layout, drilling, temporary casing or drilling fluid as required, hole stabilization, tendon fabrication and installation, centralizers, spacers, corrosion protection, bond-breakers, sheathing, trumpets, bearing plates, wedges, anchor heads, grout mixing and placement, staged or secondary grouting where required, stressing, load testing, lock-off, anchor cutoff, spoil handling, groundwater control, testing coordination, cleanup, and disposal. The Bidder shall include all labor, materials, equipment, supervision, survey control, access, temporary work, quality control, documentation, and incidental work required to complete the post-tensioned soil tieback anchor installation in accordance with the Contract Documents.

The Bidder shall be responsible for coordinating the post-tensioned soil tieback anchor installation with the reinforced concrete piles, slurry secant piles, reinforced concrete grade beam, wall reinforcing, drainage systems, utilities, adjacent improvements, and other construction. This shall include maintaining the required anchor location, inclination, orientation, unbonded length, bonded length, drilling diameter, tendon position, grout cover, corrosion protection, bearing plate alignment, anchor head elevation, stressing sequence, test loads, lock-off load, and connection to the supporting wall system. The Bidder shall verify that the proposed means and methods are compatible with the subsurface conditions, site access, construction sequencing, and adjacent structures.

Additional compensation will not be allowed for work necessary to complete the tieback anchors, maintain required tendon alignment and inclination, stabilize the drill holes, achieve the required bond capacity, perform proof and performance testing, regROUT anchors where permitted or required, coordinate with adjacent piles and structural elements, or integrate the anchor heads and bearing assemblies with the wall system unless specifically approved in writing by the Owner prior to performance of the work.

Construction Specification

Wire Mesh Gabions and Mattresses Twisted (Woven) or Welded Mesh

1. Scope

The work consists of furnishing, assembling, and installing rock filled wire mesh gabion baskets and mattresses.

2. Types

Gabions shall consist of rectangular wire mesh formed containers filled with rock. Gabions will conform to one of the following types:

Woven mesh-Nonraveling, double twisted, hexagonal wire mesh consisting of two wires twisted together in two 180-degree turns.

Welded mesh-Welded-wire mesh with a uniform square or rectangular pattern and a resistance weld at each intersection. The welded wire connections shall conform with the requirements of ASTM A 185, including wire smaller than W1.2 (0.124 in.), except that the welded connections shall have a minimum average shear strength of 70 percent and a minimum shear strength of 60 percent of the minimum ultimate tensile strength of the wire.

Gabions-Gabions shall be furnished as baskets or mattresses as specified in section 7. Baskets and mattresses shall be fabricated within a dimension tolerance of plus or minus 5 percent.

Baskets-Baskets are at least 12 inches high.

Mattresses-Mattresses are no more than 12 inches thick.

3. Material

Gabions shall be fabricated, assembled, and installed in accordance with the nominal wire sizes and dimensions shown in tables 64-1 and 64-2, using the following materials unless otherwise specified in section 7.

Wire for fabrication and assembly shall be hot-dipped galvanized. The wire shall have a minimum tensile strength of 60,000 pounds per square inch. Galvanized steel wire shall conform to ASTM A 641, class 3, soft temper.

When epoxy or polyvinyl chloride (PVC) coated wire is specified in section 7, the galvanized wire shall be coated by fusion bonded epoxy; fusion bonded, extruded; or extruded and bonded PVC material. The wire coating shall be black, gray, green, or silvery, and the initial properties of the PVC coating shall meet the following requirements:

- a. Specific gravity. In the range of 1.30 to 1.40, ASTM D 792.
- b. Abrasion resistance. The percentage of weight loss shall be less than 12 percent when tested according to ASTM D 1242, method B, at 200 cycles, CSI-A abrader tape, 80 grit.
- c. Brittleness temperature. Not higher than 15 degrees F, ASTM D 746.
- d. Tensile strength. Extruded coating (not less than 2,980 lb/in², ASTM D 412); fusion bonded coating (not less than 2,275 lb/in², ASTM D 638).
- e. Modulus of elasticity. Extruded coating (not less than 2,700 lb/in² at 100 percent strain, ASTM D 412); fusion bonded coating (not less than 1,980 lb/in² at 100 percent strain, ASTM D 638).

- f. Ultraviolet light exposure. An exposure period of not less than 3,000 hours at 63 degrees centigrade, ASTM G 152.
- g. Salt spray test. A test period of not less than 3,000 hours, ASTM B 117.

After the exposure to ultraviolet light and the salt spray test as specified above, the PVC coating shall not show cracks, blisters, splits, nor noticeable change of coloring (surface chalk). In addition, the specific gravity shall not change more than 6 percent, resistance to abrasion shall not change more than 10 percent, tensile strength shall not change more than 25 percent, and modulus of elasticity shall not change more than 25 percent from their initial values.

The wire sizes shown in tables 64-1 and 64-2 are the size of the wire after galvanizing and before coating with PVC.

Table 64-1 Minimum requirements*

Gabion baskets-height 12, 18, or 36 inches; length as specified

Type of wire	Mesh size (in)	Wire diameter (in)	PVC coating (in)	Total diameter (in)	Galvanized coating (oz./ft ²)
Woven mesh	3.25 x 4.5	0.118	None	0.118	0.80
	3.25 x 4.5	0.105	0.02	0.145	0.80
Selvage		0.153	None	0.153	0.80
		0.132	0.02	0.172	0.80
Lacing and internal connecting wire		0.086	0.02	0.126	0.70
Welded	3 x 3	0.118	None	0.118	0.80
Mesh	3 x 3	0.105	0.02	0.145	0.80
Spiral binder		0.105	0.02	0.145	0.80

Table 64-2 Minimum requirements*

Gabion mattresses-height 6, 9, or 12 inches; length as specified

Type of wire	Mesh size (in)	Wire diameter (in)	PVC coating (in)	Total diameter (in)	Galvanized coating (oz./ft ²)
Woven mesh	2.5 x 3.25	0.086	0.02	0.126	0.70
Selvage		0.105	0.02	0.145	0.80
Lacing and internal connecting wire		0.086	0.02	0.126	0.70
Welded mesh	1.5 x 3	0.080	0.02	0.120	0.70
Spiral binder		0.105	0.02	0.145	0.80

*Note: The wire sizes and PVC coating thickness shown are nominal sizes. The wire sizes include the galvanizing coating thickness.

Spiral binders are the standard fastener for welded-mesh gabion baskets and mattresses, and shall be formed from wire meeting the same quality and coating thickness requirements as specified for the gabion baskets and mattresses.

Alternate fasteners for use with wire mesh gabions, such as ring fasteners, shall be formed from wire meeting the same quality and coating thickness requirements as specified for the gabions and, as a minimum, shall conform to the manufacturer's recommendations.

Standard fasteners and alternate fasteners must provide a minimum strength of 1,400 pounds per lineal foot for gabion baskets and 900 pounds per lineal foot for gabion mattresses. When used to interconnect gabion baskets or mattresses with PVC coating, ring fasteners shall be made of stainless steel and spiral fasteners will be PVC coated. All fasteners shall meet all of the closing requirements of the gabion manufacturer in addition to any requirements specified in section 7.

Rock shall conform to the quality requirements in Maine Construction Specification 461, Rick Riprap, unless otherwise specified in section 7. At least 85 percent of the rock particles, by weight, shall be within the predominant rock size range.

Gabion basket or mattress height	Predominant rock size (in)	Minimum rock dimension (in)	Maximum rock dimension (in)
12-, 18-, or 36-inch basket	4 to 8	4	8
6-, 9-, or 12-inch mattress	3 to 6	3	6

At least 30 days before delivery to the site, the contractor shall inform the engineer in writing of the source from which the rock will be obtained. The test data and other information by which the material was determined by the contractor to meet the specification are included. The contractor shall provide the engineer free access to the source for the purpose of obtaining samples for testing and source approval.

Bedding or filter material, when specified, shall meet the gradation shown on the plans, or as specified in section 7, and the requirements of Maine Construction Specification 423 Earth Fill and Gravel Fill. Geotextile, when specified, shall conform to the requirements specified in section 7 and those of Maine Construction Specification 495, Geotextile.

4. Foundation preparation

The foundation on which the gabions are to be placed shall be cut or filled and graded to the lines and grades shown on the drawings. Surface irregularities, loose material, vegetation, and all foreign matter shall be removed from the foundation. When fill is required, it shall consist of material conforming to the specified requirements. Gabions and bedding or specified geotextiles shall not be placed until the foundation preparation is completed and the subgrade surfaces have been inspected and approved by the COTR.

Compaction of bedding or filter material is required as specified in section 7. The surface of the finished material shall be to grade and free of mounds, dips, or windrows. Geotextile shall be installed in accordance with the requirements of Maine Construction Specification 495, Geotextile.

5. Assembly and placement

Unless otherwise specified in section 7, the assembly and placement of gabions shall be in accordance with the following procedures:

Assembly-Rotate the gabion panels into position and join the vertical edges with fasteners for gabion assembly. Where lacing wire is used, wrap the wire with alternating single and double half-hitches at 4- to 5-inch intervals. Where spiral fasteners are used for welded-wire mesh, crimp the ends to secure the spirals in place. Where ring type alternate fasteners are used for basket assembly, install the fasteners at a maximum spacing of 6 inches. Use the same fastening procedures to install interior diaphragms where they are required.

Interior diaphragms are required where any inside dimension exceeds 3 feet. Diaphragms are installed to assure that no open intervals are present that exceed 3 feet.

Placement-Place the empty gabions on the foundation and interconnect the adjacent gabions along the top, bottom, and vertical edges using lacing wire. Wrap the wire with alternating single and double half-hitches at 4 to 6-inch intervals. Unless otherwise specified in section 7, lacing wire will be the only fastener allowed for interconnecting woven mesh gabions. Spiral fasteners are commonly used for the assembly and interconnection of welded mesh gabions. Spirals are screwed down at the connecting edges then each end of the spiral is crimped to secure it in place. Lacing may be used as needed to supplement the interconnection of welded mesh gabions and the closing of lids.

Interconnect each layer of gabions to the underlying layer of gabions along the front, back, and sides. Stagger the vertical joints between the gabions of adjacent rows and layers by at least half of a cell length.

6. Filling operation

After adjacent empty woven wire gabion units are set to line and grade and common sides properly connected, they shall be placed in straight line tension and stretched to remove any kinks from the mesh and to gain a uniform alignment. Welded-mesh gabions do not require stretching. The gabions may be staked to maintain the established proper alignment before the rock is placed. No stakes shall be placed through geotextile material. Connecting lacing wire and other fasteners (as allowed) shall be attached during the filling operation to preserve the strength and shape of the structure.

Internal connecting crosstie wires shall be placed in each unrestrained gabion cell of more than 18 inches in height, including gabion cells left temporarily unrestrained. Two internal connecting wires shall be placed concurrently with rock placement at each 12-inch interval of depth. In woven mesh gabions these crossties are placed evenly spaced along the front face and connecting to the back face. All crosstie wires shall be looped around two mesh openings and each wire end shall be secured by a minimum of five 180-degree twists around itself after looping.

In welded mesh gabions these crossties or stiffeners are placed across the corners of the gabions (at 12 inches from the corners) providing diagonal bracing. Lacing wire or preformed hooked wire stiffeners may be used.

The gabions shall be carefully filled with rock by machine or hand methods to ensure alignment, avoid bulges, and provide a compact mass that minimizes voids. Machine placement requires supplementing with hand work to ensure the desired results. The cells in any row shall be filled in stages so that the depth of rock placed in any one cell does not exceed the depth of rock in any adjoining cell by more than 12 inches. Along the exposed faces, the outer layer of stone shall be carefully placed and arranged by hand to ensure a neat, compact placement with a uniform appearance.

The last layer of rock shall be uniformly leveled to the top edges of the gabions. Lids shall be stretched tight over the rock filling using only approved lid closing tools as necessary. The use of crowbars or other single point leverage bars for lid closing is prohibited as they may damage the baskets. The lid shall be stretched until it meets the perimeter edges of the front and end panels. The gabion lid shall then be secured to the

sides, ends, and diaphragms with spiral binders, approved alternate fasteners, or lacing wire wrapped with alternating single and double half-hitches in the mesh openings.

Any damage to the wire or coatings during assembly, placement, and filling shall be repaired promptly in accordance with the manufacturer's recommendations or replaced with undamaged gabion baskets.

7. Payment

This bidder shall include in the proposal the sum to cover the material, rock, preparation, assembly and filling and closing of the gabion walls associated with the project as set forth in the Contract Documents.



R3 Geotechnical Engineers

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Project No.: 1031-C-25-GLE

July 31, 2026

Scotts Valley Water District
2 Civic Center Drive
Scotts Valley, CA

Attn: Nate Gillespie

Subject: Addendum 1 to the Geotechnical Investigation

Project: Proposed Slope Stabilization Wall
Glenwood Drive Water Tank
Scotts Valley, CA
APN: 023-241-13

To Mr. Gillespie:

At your request, R3 Geotechnical Engineers (R3GE) has completed an addendum to the geotechnical design criteria contained in the original geotechnical investigation prepared by Haro, Kasunich & Associates, Inc. (HKA), dated July 20, 2023, for the proposed Glenwood Water Tank slope stabilization project. I was the licensed engineer of record who signed the geotechnical report while employed at HKA.

The purpose of this addendum is to update the project to the requirements of the 2025 California Building Code (CBC), revised the slope stability model, and provide revised geotechnical design criteria and recommendations for the proposed secant pile retaining wall.

Except as specifically superseded by this addendum, the findings, conclusions, recommendations, and design criteria contained in the original geotechnical investigation remain applicable.

The following items have been updated:

1. Seismic design criteria in accordance with the 2025 California Building Code and ASCE 7-22.
2. Static and Pseudo-static slope stability evaluation.
3. Foundation and Lateral earth pressure recommendations for design of the secant pile stabilization wall.
4. Tieback bond stress.
5. Preparation of this addendum letter.

1. Seismic Design Criteria

Seismic design parameters were evaluated in general accordance with the 2025 California Building Code (CBC) and ASCE 7-22 using project site coordinates and mapped seismic hazard values obtained from the seismic design maps. Site classification was evaluated based on estimated shear wave velocity derived from Standard Penetration Test (SPT) correlations in accordance with ASCE 7-22 Section 20.3, where direct shear wave velocity measurements are not available. The site is interpreted to range between Site Class CD-D.

Where the estimated shear wave velocity range resulted in differing site classifications, the governing seismic response parameters were conservatively selected by adopting the most critical values associated with the evaluated Site Classes CD and D in accordance with ASCE requirements. Accordingly, the adopted seismic design criteria represent a conservative envelope of the governing seismic response parameters associated with the anticipated range of subsurface conditions.

Parameter	Value
Mapped Spectral Acceleration, Short Period, S_s	1.93 g
Mapped Spectral Acceleration, 1-second Period, S_1	0.75 g
MCE Site Spectral Response Acceleration, Short Period, S_{MS}	2.10 g
MCE Site Spectral Response Acceleration, 1-second Period, S_{M1}	2.25 g
Design Spectral Response Acceleration, Short Period, S_{DS}	1.40 g
Design Spectral Response Acceleration, 1-second Period, S_{D1}	1.50 g
Site-Modified Peak Ground Acceleration, PGA_M	0.77 g

Table 1: Seismic Design Criteria

The seismic parameters presented above are intended for structural design of the proposed foundation system. These parameters should be reviewed and confirmed by the project Structural Engineer based on the final building configuration, risk category, and structural design requirements.

2. Revised Slope Stability

2.1 Methodology

Static limit equilibrium slope stability analyses were performed using GeoStudio 2025.2.1 SLOPE/W with the Morgenstern-Price general limit equilibrium method. Random slip surface searches were performed to identify the critical failure surfaces for Cross Section AA presented in the original geotechnical investigation.

The subsurface conditions, slope geometry, groundwater assumptions, material properties, and geotechnical design parameters used in the original analysis remain unchanged. The only modification incorporated into this addendum is the updated horizontal seismic coefficient (K_h), which was revised based on the reduced Maximum Considered Earthquake Geometric Mean Peak Ground Acceleration (PGA_M) determined in accordance with the 2025 California Building Code (CBC) and ASCE 7-22 seismic design provisions. The updated seismic design criteria result in an approximately 35 percent reduction in PGA_M relative to the values adopted in the original geotechnical report.

Consistent with the original geotechnical investigation and current geotechnical engineering practice, a minimum Factor of Safety of 1.5 was considered acceptable for static loading conditions and 1.0 for pseudo-static seismic loading. Factors of Safety below these values do not necessarily indicate imminent slope failure but may warrant additional evaluation, mitigation, or performance-based design.

2.2 Seismic Design Parameters

The horizontal seismic coefficient (k_h) used in the pseudo-static slope stability analyses was developed based on the updated seismic design criteria of the 2025 California Building Code (CBC). The Maximum Considered Earthquake Geometric Mean Peak Ground Acceleration (PGA_M) was determined using the CBC seismic design maps for the project site and a conservative Site Class CD, resulting in a PGA_M of 0.77g. The design earthquake magnitude of $M_w = 7.5$ was obtained from deaggregation of the U.S. Geological Survey (USGS) Unified Hazard Tool.

The horizontal seismic coefficient (k_h) was determined using the procedure presented by Blake et al. (2002), *Analysis of Earthquake-Induced Landslide Hazards*, Chapter 5 of California Geological Survey Special Publication 117A (2008). Based on the updated seismic design parameters, a horizontal seismic coefficient of $k_h = 0.27$ was adopted for the pseudo-static slope stability analyses. The revised seismic coefficient supersedes the value presented in the original geotechnical report and forms the basis for the updated pseudo-static slope stability analyses presented herein.

2.3 Geotechnical Model

The subsurface conditions, stratigraphy, groundwater assumptions, material strength parameters, and slope geometry used in the updated analyses are unchanged from those presented in the original geotechnical investigation. The only modification incorporated into the updated slope stability analyses is the revised horizontal seismic coefficient (k_h) based on the updated 2025 California Building Code seismic design criteria.

2.4 Analysis Results

The results of the updated slope stability analyses are summarized in Table 2-4. Detailed SLOPE/W output and critical failure surfaces are provided in Appendix A.

Analysis Case	Cross Section	Figure No.:	Condition	Calculated FS	Min. Required FS
Existing	AA	A1	Static	0.657	1.50
Existing	AA	A2	Pseudo-static	0.901	1.00
Existing – Proposed	AA	A3	Static	1.622	1.50
Existing – Proposed	AA	A4	Pseudo-static	1.447	1.00

Table 2: SLOPE/W Analysis Results

The updated analyses confirm the overall conclusions of the original geotechnical investigation. The existing slope does not satisfy the recommended minimum factors of safety under either static or pseudo-static loading conditions, while the proposed secant pile stabilization wall provides acceptable stability under both loading cases.

The principal change resulting from the updated 2025 CBC seismic design criteria is a reduction in the required lateral resisting force that must be provided by the secant pile stabilization wall. Based on the updated pseudo-static analysis, the required lateral resisting force is approximately 7,500 pounds per

linear foot of wall, compared to 15,000 pounds per linear foot reported in the original geotechnical investigation.

Accordingly, the secant pile stabilization wall should be designed to provide a minimum lateral resisting capacity of 7,500 pounds per linear foot. Except as modified herein, the conclusions, recommendations, and design criteria presented in the original geotechnical investigation remain applicable.

3. Lateral Design Loads

The updated lateral design criteria presented herein are based on the revised slope stability analyses performed using the 2025 California Building Code seismic design parameters. The recommended design loads should be used for structural design of the secant pile stabilization wall. The Structural Engineer shall evaluate the wall for the applicable load combinations and determine the required pile diameter, embedment, reinforcement, tieback loads (if applicable), and structural capacity.

Design Condition	Backslope / Frontslope Condition	Design Value
Active, Free to Yield	Level	30 pcf (EFW)
Active, Restrained Condition	Level	20H psf (Rectangular Distribution)
Seismic	Level	10H psf (Rectangular Distribution)

Table 3: Lateral Earth Pressure

Notes:

1. Equivalent fluid weights (EFW) should be applied as triangular lateral earth pressure distributions over the retained height of the wall.
2. The restrained lateral pressure should be applied below the tieback elevation. Active lateral earth pressure may be used above the tieback elevation.
3. The seismic earth pressure increment should be applied as a uniform rectangular pressure distribution over the retained height of the wall, with the resultant acting at 0.6H above the base of the wall. The seismic increment should be added to the applicable static earth pressure condition.
4. Surcharge loads from structures, hardscape, vehicles, stockpiles, or other imposed loads should be evaluated by the Structural Engineer and added to the recommended earth pressures, as appropriate.

4. Tieback Design Criteria

Where required by the structural design, tiebacks may be incorporated into the secant pile stabilization wall system to satisfy structural strength and serviceability requirements. Tiebacks should be designed by the project structural engineer using the updated wall design loads presented in this addendum.

For tiebacks with bonded lengths developed within the highly weathered Santa Cruz Mudstone, an allowable design bond stress of 4,800 psf may be used, subject to successful verification by proof and/or

performance testing during construction. The allowable bond stress should be applied only to the portion of the bonded length embedded within the highly weathered Santa Cruz Mudstone.

Tieback proof and performance testing should be performed in accordance with the project specifications and applicable PTI requirements. If field testing does not verify the recommended bond stress, the tieback design should be revised using the verified field capacity.

Except for the revised allowable bond stress presented herein, the tieback diameter, inclination, minimum bonded and unbonded lengths, installation requirements, and other recommendations presented in the original geotechnical investigation remain applicable.

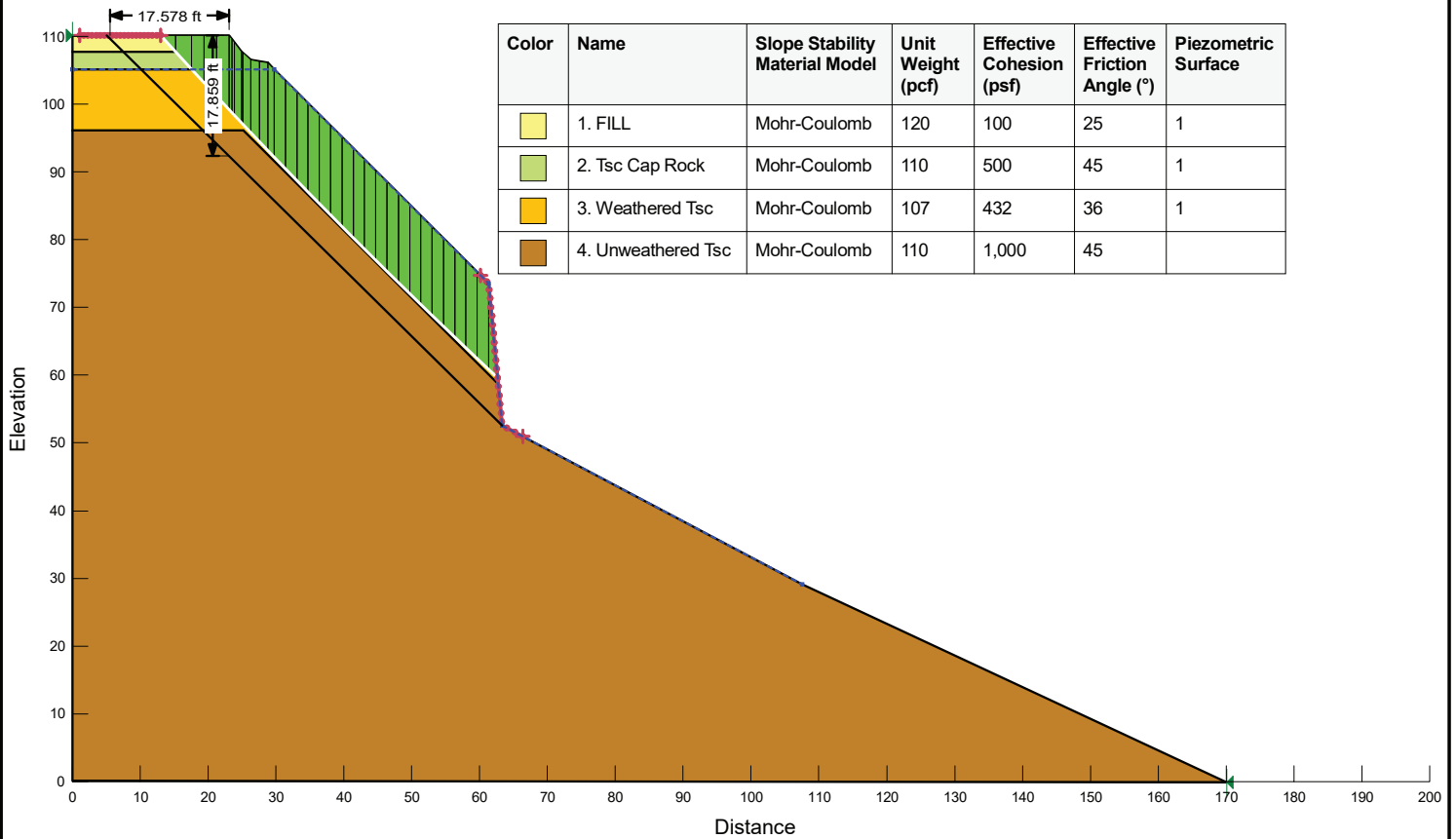
Should you have any questions or require additional information, please contact me.

Sincerely,

Ashton J. Buckner, P.E. 93365
Principal Engineer
R3 Geotechnical Engineers



APPENDIX A
Slope Stability Results



R3 Geotechnical Engineers

1. EXISTING - STATIC

Factor of Safety: 0.657

Horz Seismic Coef.: 0

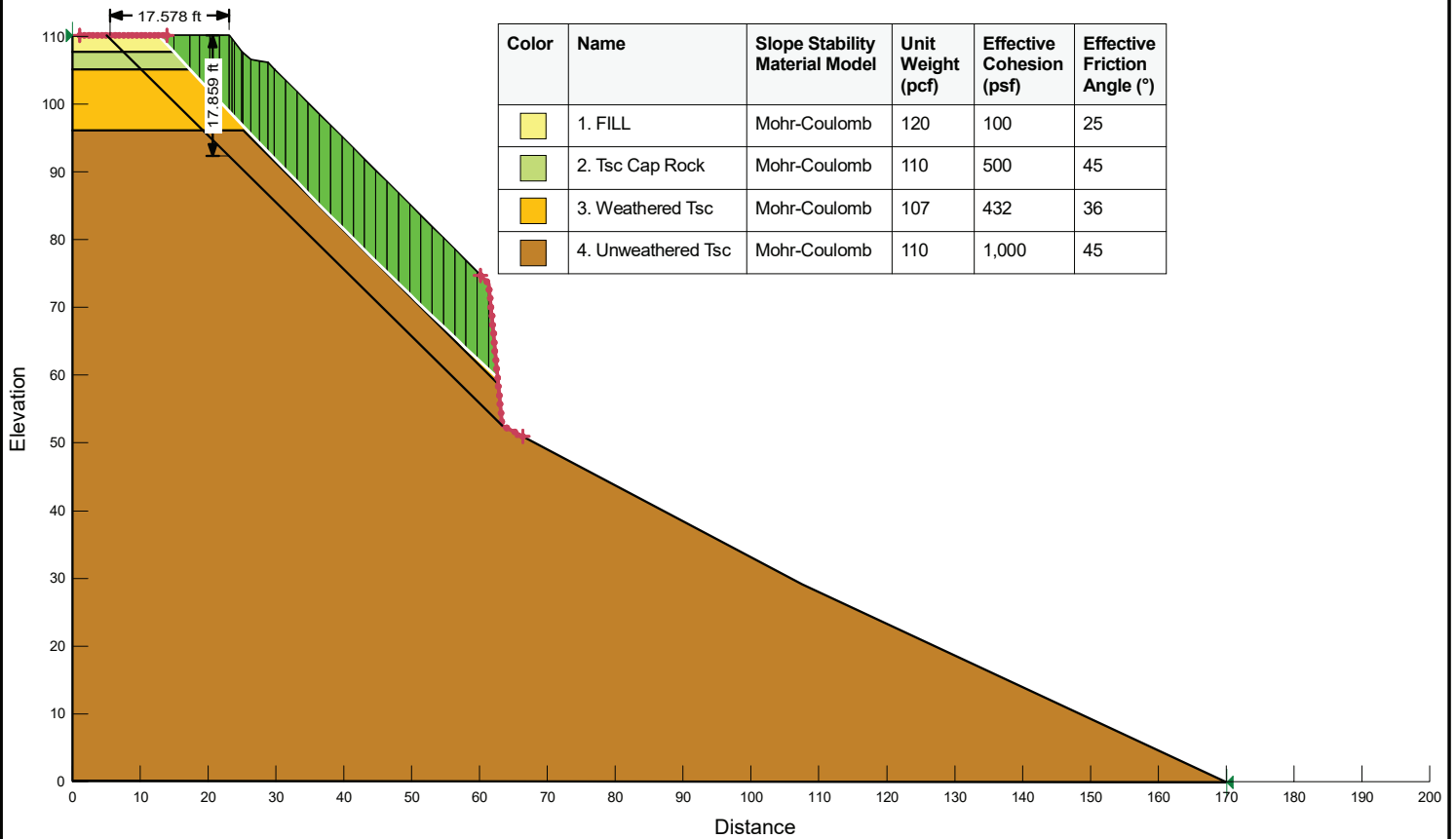
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Project: 2026 GLENWOOD TANK

Figure No.: A1



R3 Geotechnical Engineers

2. EXISTING - SEISMIC

Factor of Safety: 0.901

Horz Seismic Coef.: 0.27

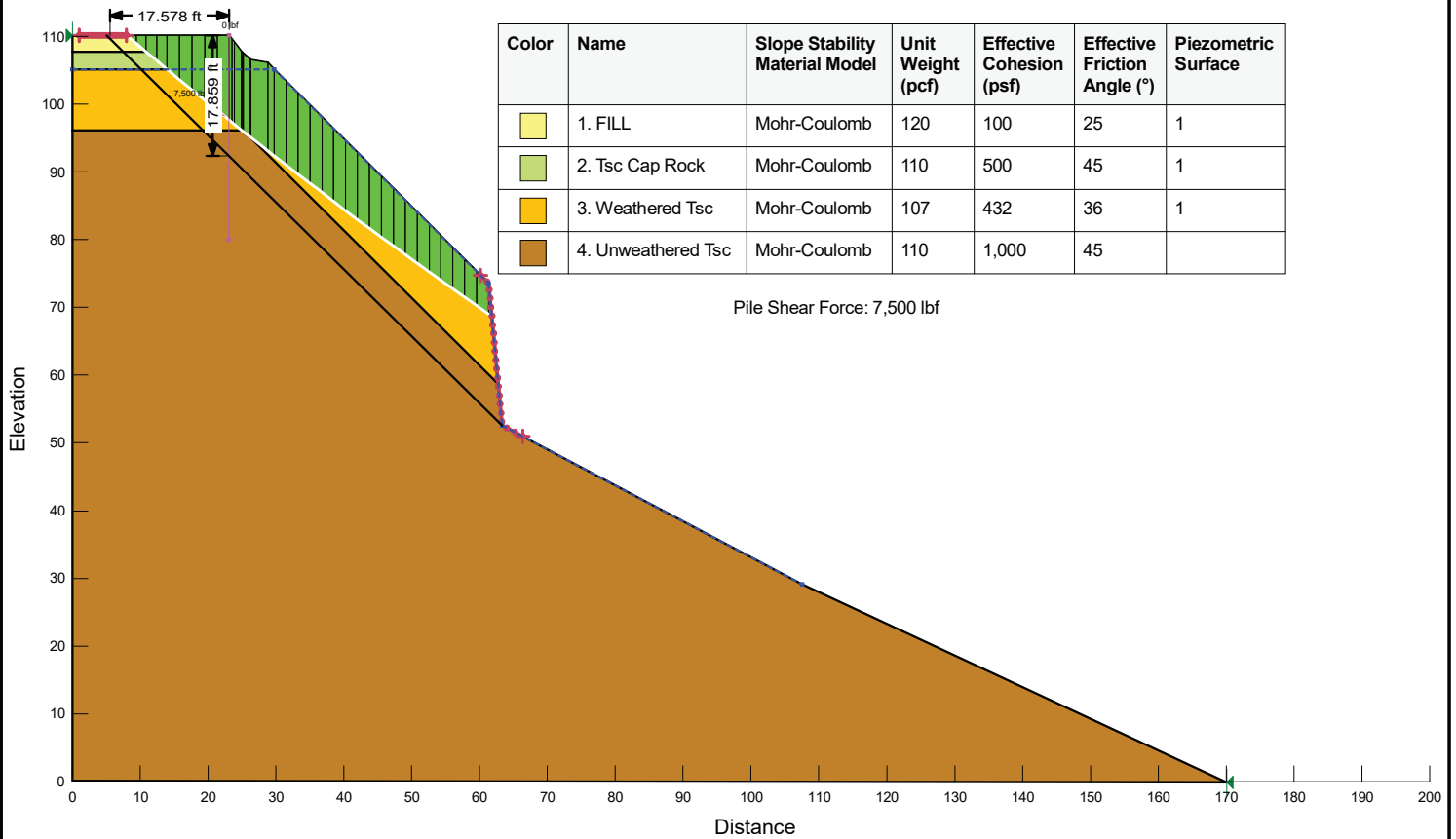
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Project: 2026 GLENWOOD TANK

Figure No.: A2



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3. PROPOSED - STATIC

Factor of Safety: 1.622

Horz Seismic Coef.: 0

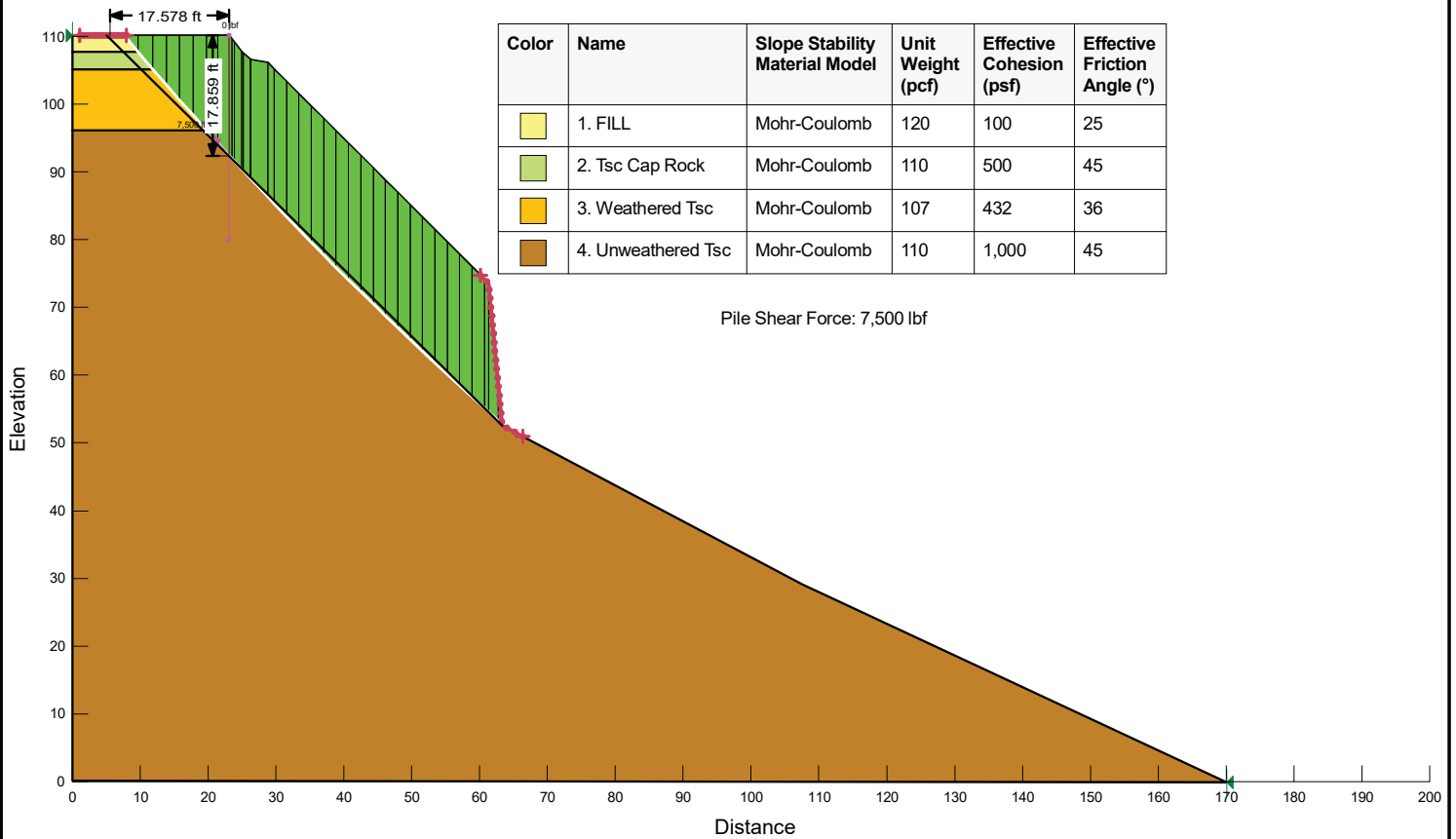
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Figure No.: A3



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4. PROPOSED - SEISMIC

Factor of Safety: 1.447

Horz Seismic Coef.: 0.27

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Project: 2026 GLENWOOD TANK

Figure No.: A4